Power control-based fuzzy and modulated hysteresis methods for micro-grid using a photovoltaic system

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Abstract— This paper discusses the smart grid integration of a photovoltaic system. Several methods can be applied for controlling the power injected into the grid by a photovoltaic system. These techniques ensure that the system operates safely and efficiently, and that the power levels are maintained within the required limits. Maximum power point tracking based on fuzzy logic control (FLC) is incorporated into the inverter control in our work. The inverter keeps the power factor by managing the reactive power while controlling the voltage and frequency of the photovoltaic system. Although the hysteresis current control is a useful technique, it has its limitations, particularly when it comes to the frequency control. In the present study, a modulated hysteresis control (MHC) was applied, to ensure that the inverter operates at a constant switching frequency, enhancing the efficiency of the system. The study was done using the Matlab software, and the findings demonstrate that the MHC-studied system supplied low-harmonic energy to a utility grid.

Keywords— Grid, Photovoltaic, FLC MPPT, Power control.

I. INTRODUCTION

Smart grid integration of photovoltaic systems is an important step towards a more sustainable and efficient electrical grid. Due to its many benefits, including its durability and availability in many parts of the world, photovoltaic energy has become increasingly important in electrical applications. However, the power output of photovoltaic panels can be unpredictable as it can fluctuate throughout the day according to varying climate conditions. To address this problem, maximum power point tracking (MPPT) methods are being employed[1-2], including digital MPPT techniques [3-16]. One of the most popular digital MPPT techniques is the fuzzy logic control (FLC) [17-23].It has several advantages over other MPPT techniques, namely its ability to handle non-linear and uncertain systems, its flexibility to adapt to changing operating conditions, and its capability to provide better performance in complex systems. FLC-based MPPT systems have been utilized for various applications.

In this study, a modulated hysteresis control (MHC) is used to overcome the drawbacks of the hysteresis control current, such as a variable switching frequency. This control strategy reduces the switching losses and boosts the total efficiency of the system by adjusting the switching frequency based on the output voltage of the inverter. This control technique results in a more sinusoidal output waveform, which reduces the harmonic distortion. Also, MHC is relatively easy to implement and requires less complex control algorithms compared to other control techniques, which makes it a cost-effective solution for many applications.

The simulation findings reveal how effectively the modulated hysteresis control method operates to control the output power of the photovoltaic system. Also, the results show that the technique ensures that the inverter operates at a constant switching frequency, leading to improved efficiency and performance..

II. MODELING OF THE STUDIED SYSTEM

The studied system is represented in Fig.1. The photovoltaic generator is made up of 10 strings, each string comprising 12 panels of 80 Wp (Table 1) connected in series. The inverter includes an MPPT control. Through the incorporation of MPPT in the inverter management, the DC/AC conversion process is effective and optimized. The inverter control also includes an MHC technique to ensure that the inverter operates at a constant switching frequency.

TABLE I. . PARAMETERS OF THE PV PANEL.

Parameters	Values		
Photovoltaic power	80 Wp		
Maximum current at MPP	4.65 A		
Maximum voltage at MPP	17.5V		
Short-circuit current	4.95A		
Open-circuit voltage	21.9V		
Temperature coefficient of the short-circuit current	3 mA/°C		
Temperature coefficient of the open-circuit voltage	-150mV/°C		



Fig. 1. Studied system.

A. Photovoltaic generator

Different mathematical models can be used to calculate the electrical characteristics of a PV panel. They vary in complexity and accuracy. In our work, we used the singlediode model [1]. This model is a simple but useful tool for describing the electrical characteristics of a photovoltaic generator. The electrical current of the single-diode model is [3, 16]:

$$I_{pv} = I_{ph} - I_0 \times \left[\exp\left(\frac{q \times (V_{pv} + R_s \times I_{pv})}{A \times N_s \times K \times T_j}\right) - 1 \right] - \frac{V_{pv} + R_s \times I_{pv}}{R_{sh}}$$
(1)

where I_{ph} is the photo-current, I_d the diode-current and R_{sh} shunt resistance, I_0 the reverse saturation current of the diode, q the electron charge, k Botzman's constant, A diode ideality factor and N_s the serial number of cells.

Photovoltaic electrical characteristics were established using the test bench displayed in Fig. 2.



Fig. 2. Test bench to determinate the electrical caracteristics.

The electrical characteristics are shown in Fig.3.



Fig. 3. Electrical characteristics of the PV panel.

B. MPPT control

The P&O algorithm is simple and effective, but it can sometimes oscillate around the maximum power point (MPP), especially if the perturbations are too large. The use of a FLC in a photovoltaic system can help to improve its performance and efficiency, making it a more reliable and cost-effective source for clean energy. The FLC generates an output reference voltage variation $V_{pv,ref}$ used to converge

to the optimal point by taking two inputs: the power variation ΔP_{pv} and the voltage variation ΔV_{pv} . The fuzzy rules are based on power variations (ΔP_{pv}) and voltage variations (ΔV_{pv}) as given in Table 2. [25].

ΔP_{pv} ΔV_{pv}	BN	MN	SN	Ζ	SP	MP	BP
BN	BP	BP	MP	Ζ	MN	BN	BN
MN	BP	MP	SP	Z	SN	MN	BN
SN	MP	SP	SP	Ζ	SN	SN	MN
Z	BN	MN	SN	Ζ	SP	MP	BP
SP	MN	SN	SN	Ζ	SP	SP	MP
MP	BN	MN	SN	Ζ	SP	MP	BP
BP	BN	BN	MN	Ζ	MP	BP	BP

TABLE II. FUZZY RULES

The MPPT algorithm is provided by using these linguistic rules [26].

$$\begin{cases} \Delta P_{pv} = P_{pv}(t) - P_{pv}(t-1) \\ \Delta V_{pv} = V_{pv}(t) - V_{pv}(t-1) \\ V_{pv-ref}(t) = V_{pv}(t-1) + \Delta V_{pv-ref}(t) \end{cases}$$
(2)

 $P_{pv}(t)$, $V_{pv}(t)$, and $V_{pv,ref}(t)$, respectively, refer to the power, voltage and reference voltage of a PV generator at a particular time t. Fig. 4 depicts the structural scheme of the fuzzy logic controller.



Fig. 4. Structural scheme of the fuzzy logic controller.

C. Proposed Power control

1) Modulated hysteresis control

By using the MHC control technique, the switching frequency of the inverter can be kept constant to reduce the switching losses. The MHC involves adding a triangular signal to the reference current, and their comparison is used to control the output of the inverter. The triangular carrier signal frequency matches the semiconductor switching frequency in the inverter. The amplitude of the triangular carrier signal is typically chosen to be small compared to the reference current signal to avoid excessive switching of the inverter. The resulting signal is compared to a hysteresis band, having a fixed range of values centered on the reference current. If the resulting signal falls outside the hysteresis band $B_{\rm H}$, the output of the inverter is adjusted to bring the signal back within the hysteresis band.

$$i_{\text{mod}-ref} = i_{ref} + i_{tr} \tag{3}$$

The triangle signal is represented by i_{tr} , while $i_{mod-ref}$ and i_{ref} are respectively the modulated reference current and the reference current.

The requirements of the system and the characteristics of the load are usually taken into consideration when choosing the bandwidth. A larger bandwidth allows a more rapid response to changes in the input signal, but may result in more switching of the converter and also in increased losses. A narrower bandwidth may reduce the switching losses but may result in a slower response to changes in the input signal. The value of the band width B_{H} is typically chosen as a compromise between these factors to optimize the performance of the system. The switching frequency is equal to the frequency of the triangular carrier signal, is typically chosen to be a multiple of the desired output frequency. In order to maintain a constant switching frequency and minimize the switching losses [4], the measured current variation during half a period of the triangular signal should not exceed the difference between the upper and lower limits. These limits define the switching times of the voltage inverter when the measured current intersects only the hysteresis band limits (Fig. 5) for each twice half-period $T_{tr}/2$ of the triangular signal.



Fig. 5. States of the switches in MHC.

2) Power control

It is based on controlling the power factor by maintaining it to the unit factor, and controlling active power flow to eliminate reactive power. A PI controller, used to control the direct bus voltage, generates a reference value for the active power, is then used to adjust the output power of the power converter. The reference current is produced by dividing the active power reference by the grid capacitance. Thus a reference current is generated corresponding to the amount of current required to supply the grid with the intended active power:

$$i_{inv} = S_1 i_a + S_2 i_b + S_3 i_c \tag{4}$$

where (i_a, i_b, i_c) are the grid currents and S_i (*i*=1, 2, 3) are the logic functions.

Also, the voltages inverter (v_1, v_2, v_3) are defined by:



Fig. 6. Studied system configuration

$$\begin{pmatrix} v_1 \\ v_2 \\ v_3 \end{pmatrix} = \frac{V_{pv}}{3} \begin{pmatrix} -2 & 1 & 1 \\ 1 & -2 & 1 \\ 1 & 1 & -2 \end{pmatrix} \begin{pmatrix} S_1 \\ S_2 \\ S_3 \end{pmatrix}$$
(5)

Using the filter, which is constituted of a resistance R_g and an inductance L_g , the phase voltages of the grid are generated:

$$\begin{pmatrix} v_1 \\ v_2 \\ v_3 \end{pmatrix} = R_g \begin{pmatrix} i_a \\ i_b \\ i_c \end{pmatrix} + L_g \frac{d}{dt} \begin{pmatrix} i_a \\ i_b \\ i_c \end{pmatrix} + \begin{pmatrix} E_1 \\ E_2 \\ E_3 \end{pmatrix}$$
(6)

Fig. 6 shows the control system for the inverter and the grid connection. The unit power factor can be set to zero reactive power and the supplied active power to its reference to adjust the direct bus voltage and generate the current reference based on the capacitance.

The different equations of the powers are expressed as follows:

$$\begin{cases}
P_{ref} = P_{pv} - P_c \\
P_c = I_{cref} \cdot V_{pv} \\
I_{cref} = PI(V_{dcref} - V_{dc})
\end{cases}$$

$$\begin{cases}
P_{ref} = E_d \cdot I_{adref} + E_q \cdot I_{aqref} \\
Q_{ref} = E_q \cdot I_{adref} - E_d \cdot I_{adref}
\end{cases}$$
(8)

The current references are then obtained:

$$I_{adref} = \frac{P_{ref} \cdot E_{d} + Q_{ref} \cdot E_{q}}{E_{d}^{2} + E_{q}^{2}}$$
(9)
$$I_{aqref} = \frac{P_{ref} \cdot E_{q} + Q_{ref} \cdot E_{d}}{E_{d}^{2} + E_{q}^{2}}$$

To achieve the reference power, the inverter must control the PV generator power output. P_C represents the capacitance power, which filters the output voltage of the inverter and reduces the harmonics in the system, while Q_{ref} refers to the reactive power injected or absorbed from the grid.

III. SIMULATION STUDY

The studied system was simulated under three different solar irradiance profiles (Fig.7). The FLC algorithm is used for the photovoltaic power maximization and the inverter current is controlled by using the MHC approach (A_{tt}+B_H>0.3, f=10 kHz, B_H <0.27).The proposed system consists of a photovoltaic generator with a total peak power of approximately 9.6 kW and a photovoltaic voltage of 600 V in standard test conditions (E_s=1000 W/m², cell temperature of 25°C). The photovoltaic power tracks its reference (Fig.8) across three different solar irradiance profiles.



Fig. 7. Measured solar irradiance profiles.



Fig. 8. Photovoltaic and reference powers.

Fig.9(a, b) shows the current and voltage on the grid side under the three days using the classical hysteresis control and the modulated hysteresis control. The currents in the case of the classical hysteresis present irregularities in the shape (Fig. 9-a). The total harmonic distortion (THD) is around 7.83 %. Nevertheless, for the MHC, the grid current has a smooth shape and a THD of 5.43% (Fig.9-b), and the frequency is almost steady at 50 Hz. Additionally, as can be seen in Fig. 10, the voltage and current are in phase. This implies that the maximum power extracted from the photovoltaic (PV) array is transmitted to the grid, and the system operates at a unit power factor (Fig.11) with no exchange of reactive power.





(a) Classical hysteresis control



Fig. 9. Grid current waveforms with their THD

Based on this finding, it can be concluded that when utilizing Maximum Harmonic Control (MHC), the system has the capability of supplying energy to a utility grid with reduced harmonics in comparison to the traditional control approach.



Fig. 10. Grid voltage and currentusing the MHC current.



Fig. 11. Power factor.

From these findings, it shows that the grid-connected photovoltaic system at the MPP is capable of operating continuously while supplying low harmonic and unit power factor energy to the utility grid.

IV. CONCLUSION

This paper presents a study on a grid-connected photovoltaic (PV) system controlled by fuzzy logic control (FLC). A fast and stable FLC maximum power point tracking (MPPT) controller is employed in the control system to integrate the MPPT algorithm into the inverter control, resulting in faster MPP tracking compared to traditional methods. The current control is implemented using the modulated hysteresis control (MHC) to ensure a steady switching frequency. This innovative approach utilizing fuzzy logic theory and MHC control has great potential in enhancing the performance and efficiency of PV systems, ultimately making them a more sustainable source of energy for the future. The results of the study demonstrate that the MHC controller generates lower total harmonic distortion (THD) in the grid current compared to a classical controller, indicating the potential of using fuzzy logic theory and MHC control in improving the quality of power injected into the grid. Furthermore, the research shows that the grid-connected PV system can operate continuously at the MPP while supplying low harmonic and unit power factor energy to the utility grid, highlighting the promise of this approach in improving power quality.

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